

EXHIBIT A



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Dror et al.

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(54) **MINIATURE TELEPHOTO LENS ASSEMBLY**

H04N 9/097 (2013.01); **G02B 5/005** (2013.01);
G02B 9/12 (2013.01); **G02B 9/62** (2013.01);

(71) Applicant: **Corephotonics Ltd.**, Tel-Aviv (IL)

(Continued)

(72) Inventors: **Michael Dror**, Nes-Ziona (IL);
Ephraim Goldenberg, Ashdod (IL); **Gal Shabtay**, Tel-Aviv (IL)

(58) **Field of Classification Search**

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G02B 13/18; **G02B 13/004**; **G02B 9/64**;
G02B 5/005; **G02B 13/00**; **G02B 9/12**

(73) Assignee: **Corephotonics Ltd.**, Tel-Aviv (IL)

USPC **359/713**, **714**, **715-717**, **739**, **740**,
359/745-748, **754-795**

(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

See application file for complete search history.

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(21) Appl. No.: **14/932,319**

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(Continued)

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International Search Report and Written Opinion issued in related PCT patent application PCT/IB2014/062465, dated Oct. 29, 2014, 8 pages.

Primary Examiner — Evelyn A Lester

(74) *Attorney, Agent, or Firm* — Nathan & Associates Patent Agents Ltd.; Menachem Nathan

(51) **Int. Cl.**

G02B 13/18 (2006.01)

G02B 3/02 (2006.01)

(Continued)

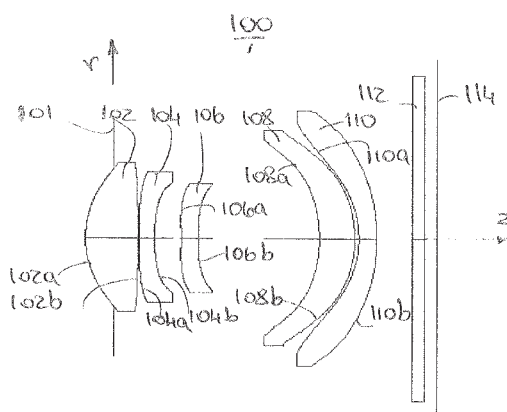
(57) **ABSTRACT**

An optical lens assembly includes five lens elements and provides a TTL/EFL<1.0. In an embodiment, the focal length of the first lens element $f_1 < \text{TTL}/2$, an air gap between first and second lens elements is smaller than half the second lens element thickness, an air gap between the third and fourth lens elements is greater than $\text{TTL}/5$ and an air gap between the fourth and fifth lens elements is smaller than about 1.5 times the fifth lens element thickness. All lens elements may be aspheric.

(52) **U.S. Cl.**

CPC **H04N 5/23296** (2013.01); **G02B 1/041** (2013.01); **G02B 9/60** (2013.01); **G02B 13/009** (2013.01); **G02B 13/0045** (2013.01); **G02B 13/02** (2013.01); **G02B 27/0025** (2013.01); **G02B 27/646** (2013.01); **H04N 5/2254** (2013.01); **H04N 5/2257** (2013.01); **H04N 5/2258** (2013.01); **H04N 9/045** (2013.01);

20 Claims, 6 Drawing Sheets



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- H04N 5/232* (2006.01)
- G02B 13/00* (2006.01)
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- H04N 9/04* (2006.01)
- H04N 9/097* (2006.01)
- G02B 13/02* (2006.01)
- G02B 1/04* (2006.01)
- G02B 27/00* (2006.01)
- G02B 27/64* (2006.01)
- G02B 9/62* (2006.01)
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- G02B 9/64* (2006.01)
- G02B 9/12* (2006.01)
- H04N 101/00* (2006.01)
- (52) **U.S. Cl.**
- CPC *G02B 9/64* (2013.01); *G02B 13/00*
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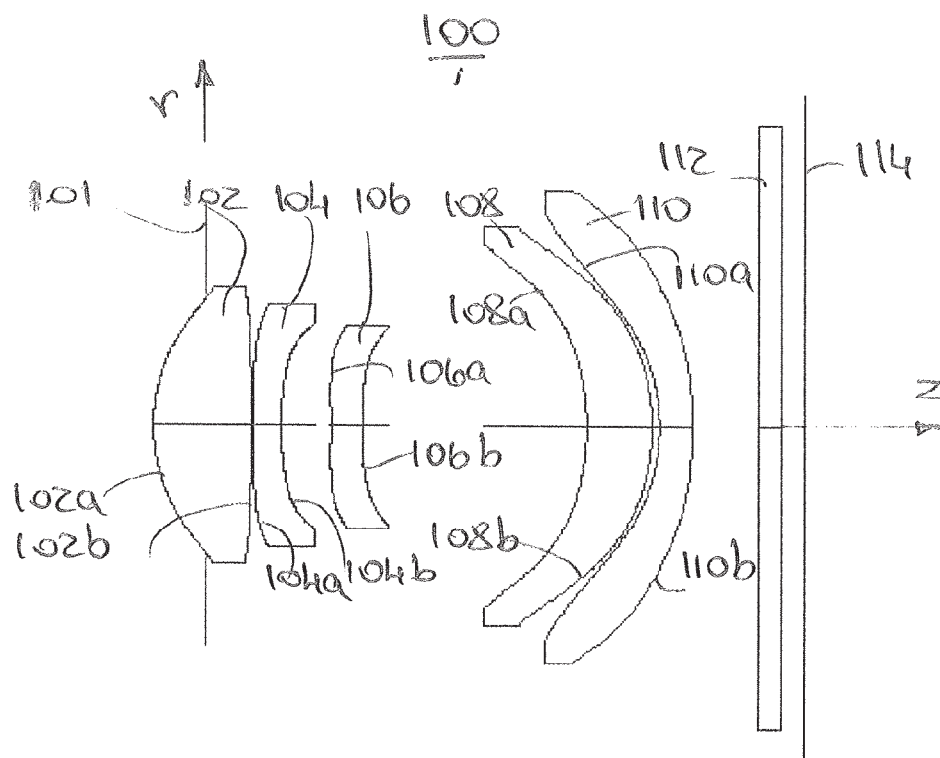


FIG. 1A

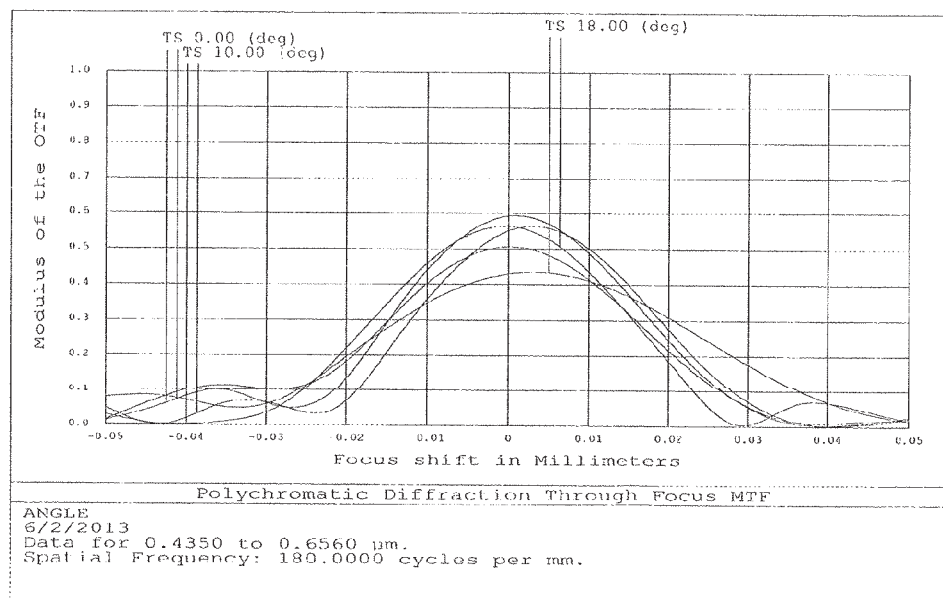


FIG. 1B

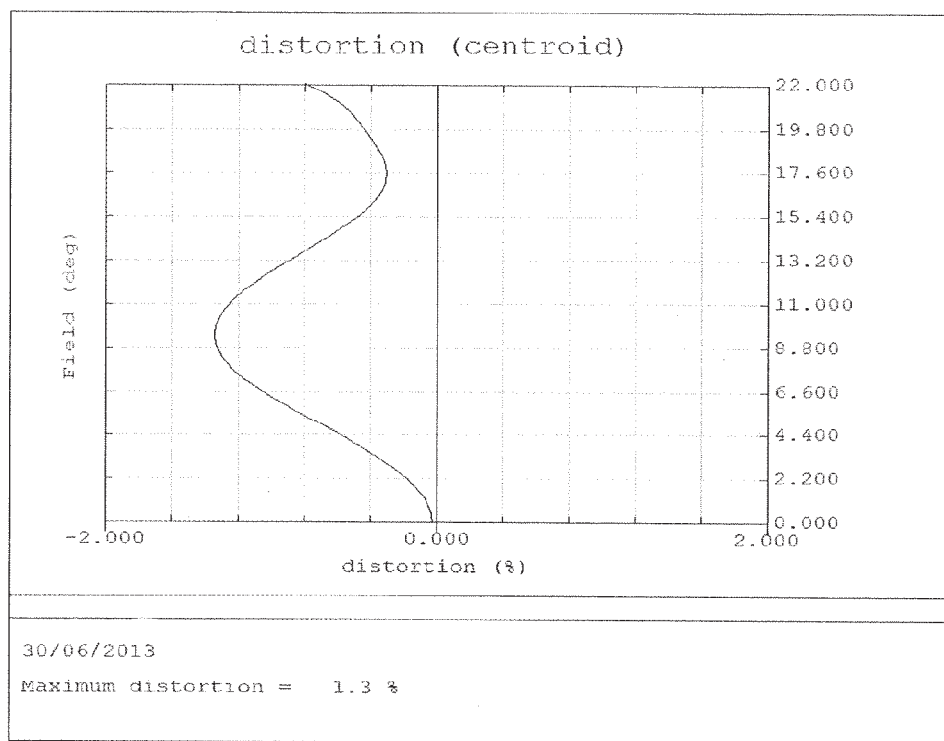


FIG. 1C

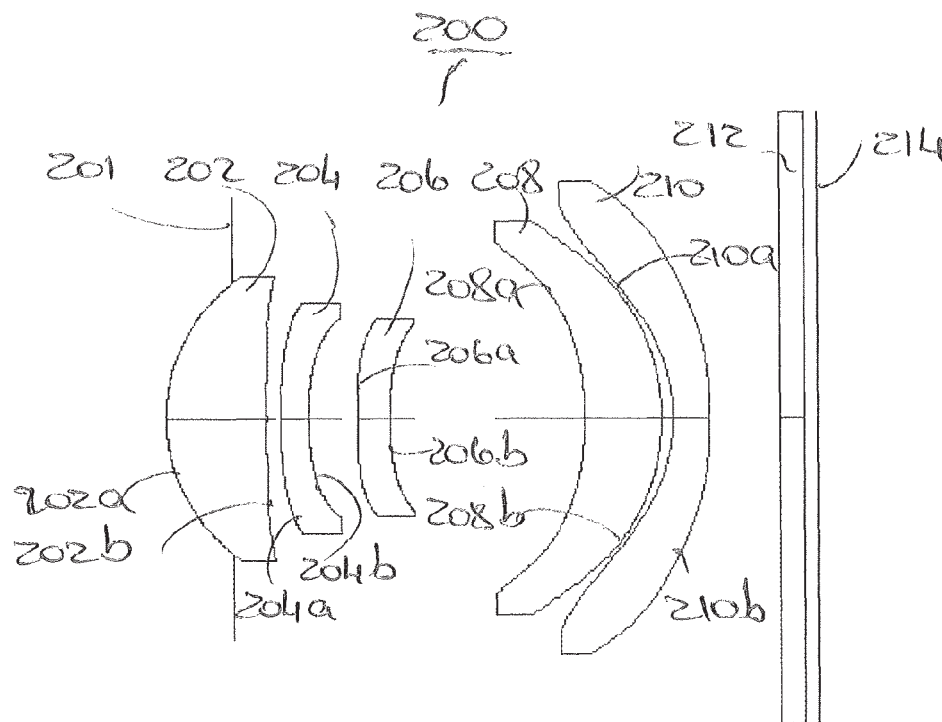


FIG. 2A

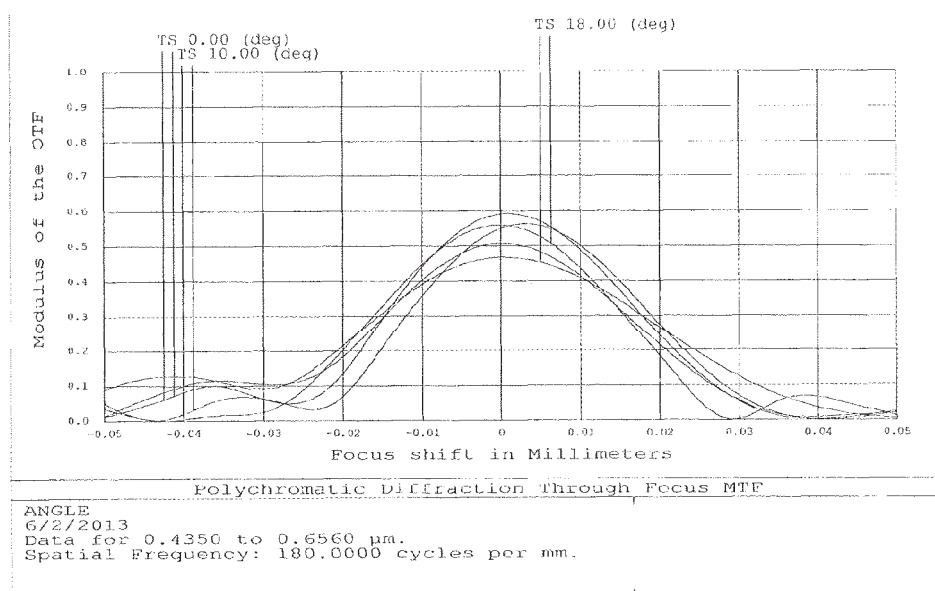


FIG.2B

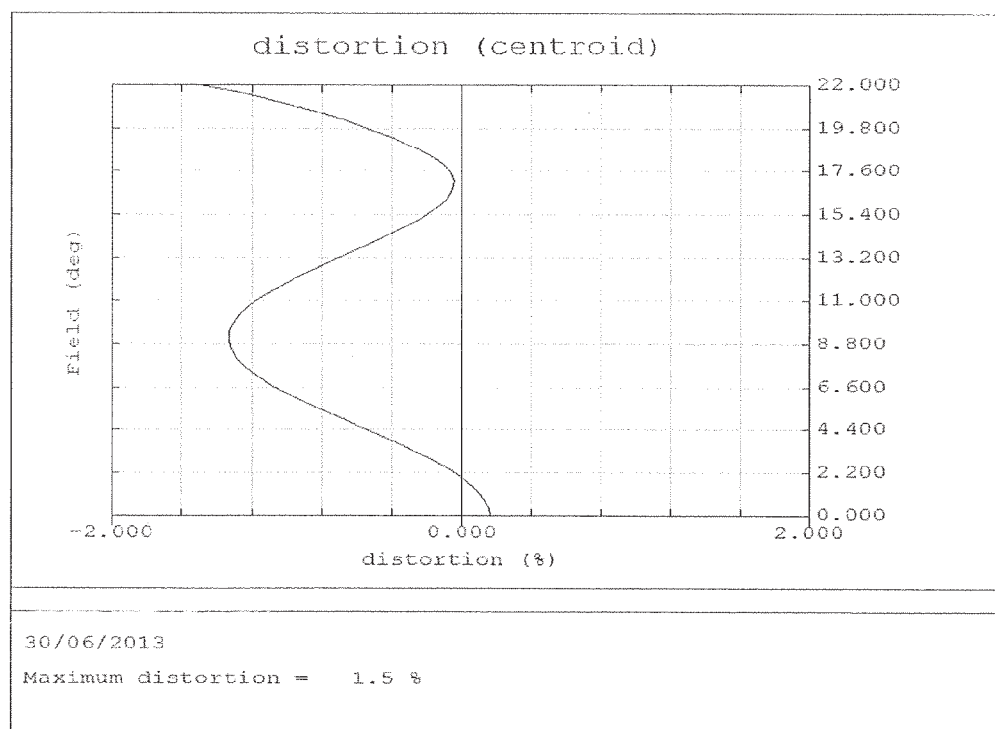


FIG. 2C

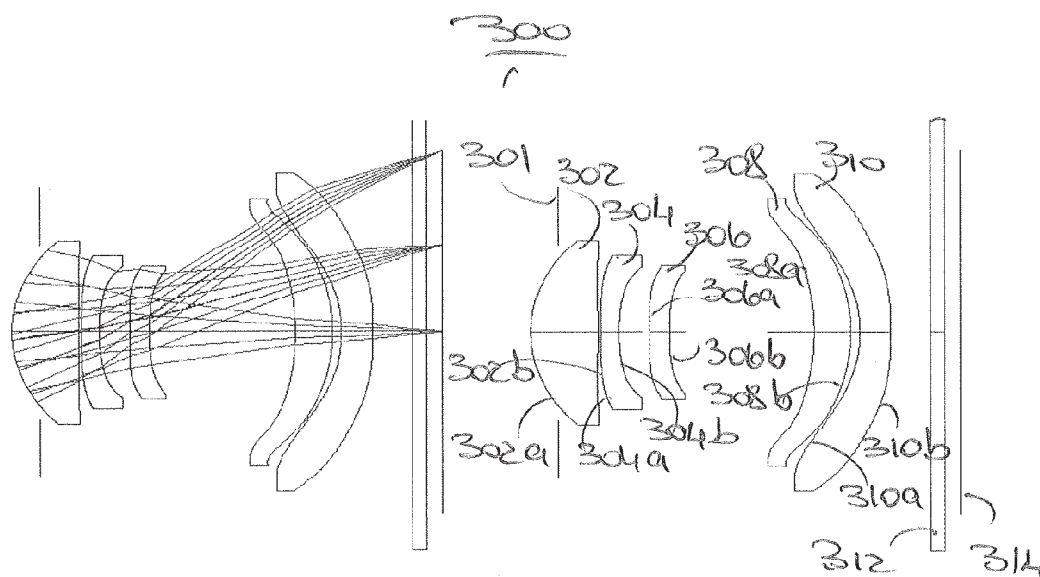


FIG. 3A

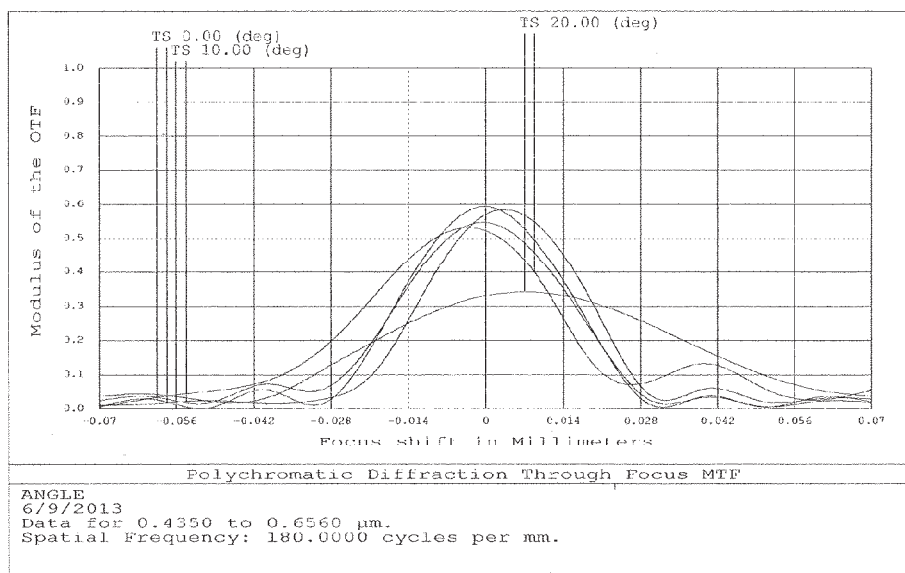


FIG. 3B

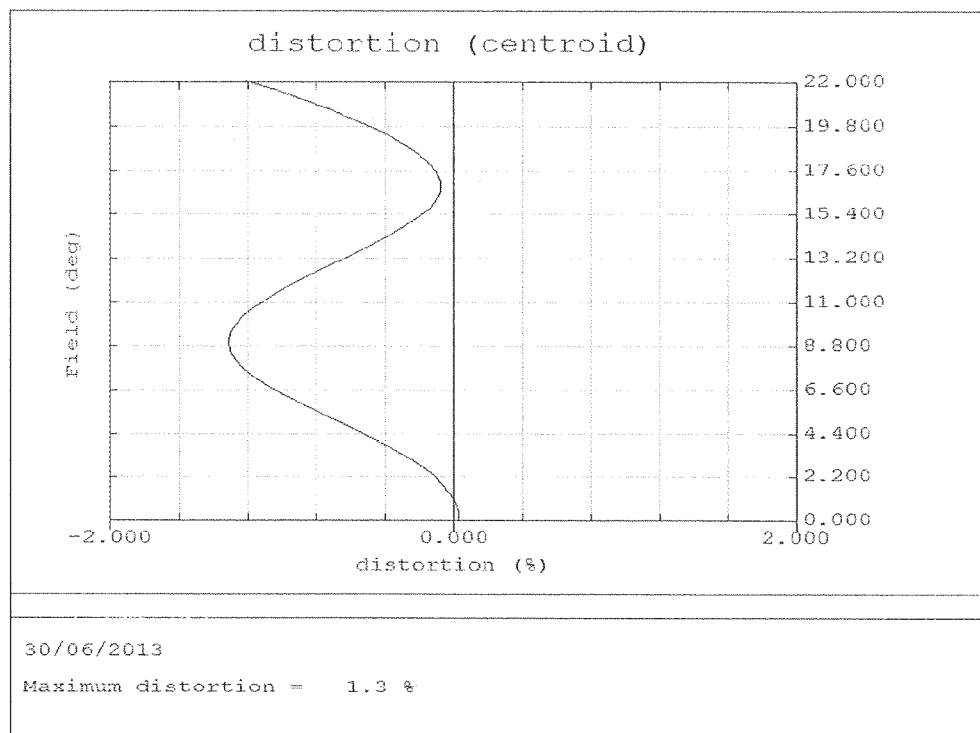


FIG. 3C

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MINIATURE TELEPHOTO LENS ASSEMBLY

CROSS REFERENCE TO RELATED APPLICATIONS

This application is a Continuation application of U.S. patent application Ser. No. 14/367,924 filed Jun. 22, 2014 which was a 371 of international application PCT/IB2014/062465 filed Jun. 20, 2014, and is related to and claims priority from U.S. Provisional Patent Application No. 61/842,987 filed Jul. 4, 2013, which is incorporated herein by reference in its entirety.

FIELD

Embodiments disclosed herein relate to an optical lens system and lens assembly, and more particularly, to a miniature telephoto lens assembly included in such a system and used in a portable electronic product such as a cellphone.

BACKGROUND

Digital camera modules are currently being incorporated into a variety of host devices. Such host devices include cellular telephones, personal data assistants (PDAs), computers, and so forth. Consumer demand for digital camera modules in host devices continues to grow. Cameras in cellphone devices in particular require a compact imaging lens system for good quality imaging and with a small total track length (TTL). Conventional lens assemblies comprising four lens elements are no longer sufficient for good quality imaging in such devices. The latest lens assembly designs, e.g. as in U.S. Pat. No. 8,395,851, use five lens elements. However, the design in U.S. Pat. No. 8,395,851 suffers from at least the fact that the TTL/EFL (effective focal length) ratio is too large.

Therefore, a need exists in the art for a five lens element optical lens assembly that can provide a small TTL/EFL ratio and better image quality than existing lens assemblies.

SUMMARY

Embodiments disclosed herein refer to an optical lens assembly comprising, in order from an object side to an image side: a first lens element with positive refractive power having a convex object-side surface, a second lens element with negative refractive power having a thickness d_2 on an optical axis and separated from the first lens element by a first air gap, a third lens element with negative refractive power and separated from the second lens element by a second air gap, a fourth lens element having a positive refractive power and separated from the third lens element by a third air gap, and a fifth lens element having a negative refractive power, separated from the fourth lens element by a fourth air gap, the fifth lens element having a thickness d_5 on the optical axis.

An optical lens system incorporating the lens assembly may further include a stop positioned before the first lens element, a glass window disposed between the image-side surface of the fifth lens element and an image sensor with an image plane on which an image of the object is formed.

The effective focal length of the lens assembly is marked "EFL" and the total track length on an optical axis between the object-side surface of the first lens element and the electronic sensor is marked "TTL". In all embodiments, TTL is smaller than the EFL, i.e. the TTL/EFL ratio is smaller than 1.0. In some embodiments, the TTL/EFL ratio is smaller than 0.9. In an embodiment, the TTL/EFL ratio is about 0.85. In all embodiments, the lens assembly has an F number $F\# < 3.2$. In

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an embodiment, the focal length of the first lens element f_1 is smaller than $TTL/2$, the first, third and fifth lens elements have each an Abbe number ("Vd") greater than 50, the second and fourth lens elements have each an Abbe number smaller than 30, the first air gap is smaller than $d_2/2$, the third air gap is greater than $TTL/5$ and the fourth air gap is smaller than $1.5d_5$. In some embodiments, the surfaces of the lens elements may be aspheric.

In an optical lens assembly disclosed herein, the first lens element with positive refractive power allows the TTL of the lens system to be favorably reduced. The combined design of the first, second and third lens elements plus the relative short distances between them enable a long EFL and a short TTL. The same combination, together with the high dispersion (low Vd) for the second lens element and low dispersion (high Vd) for the first and third lens elements, also helps to reduce chromatic aberration. In particular, the ratio $TTL/EFL < 1.0$ and minimal chromatic aberration are obtained by fulfilling the relationship $1.2 \times |f_3| > |f_2| > 1.5 \times f_1$, where "f" indicates the lens element effective focal length and the numerals 1, 2, 3, 4, 5 indicate the lens element number.

The relatively large distance between the third and the fourth lens elements plus the combined design of the fourth and fifth lens elements assist in bringing all fields' focal points to the image plane. Also, because the fourth and fifth lens elements have different dispersions and have respectively positive and negative power, they help in minimizing chromatic aberration.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1A shows a first embodiment of an optical lens system disclosed herein;

FIG. 1B shows the modulus of the optical transfer function (MTF) vs. focus shift of the entire optical lens assembly for various fields in the first embodiment;

FIG. 1C shows the distortion vs. field angle (+Y direction) in percent in the first embodiment;

FIG. 2A shows a second embodiment of an optical lens system disclosed herein;

FIG. 2B shows the MTF vs. focus shift of the entire optical lens assembly for various fields in the second embodiment;

FIG. 2C shows the distortion +Y in percent in the second embodiment;

FIG. 3A shows a third embodiment of an optical lens system disclosed herein;

FIG. 3B shows the MTF vs. focus shift of the entire optical lens system for various fields in the third embodiment;

FIG. 3C shows the distortion +Y in percent in the third embodiment.

DETAILED DESCRIPTION

In the following description, the shape (convex or concave) of a lens element surface is defined as viewed from the respective side (i.e. from an object side or from an image side). FIG. 1A shows a first embodiment of an optical lens system disclosed herein and marked 100. FIG. 1B shows the MTF vs. focus shift of the entire optical lens system for various fields in embodiment 100. FIG. 1C shows the distortion +Y in percent vs. field. Embodiment 100 comprises in order from an object side to an image side: an optional stop 101; a first plastic lens element 102 with positive refractive power having a convex object-side surface 102a and a convex or concave image-side surface 102b; a second plastic lens element 104 with negative refractive power and having a meniscus convex object-side surface 104a, with an image side surface marked

104b; a third plastic lens element **106** with negative refractive power having a concave object-side surface **106a** with an inflection point and a concave image-side surface **106b**; a fourth plastic lens element **108** with positive refractive power having a positive meniscus, with a concave object-side surface marked **108a** and an image-side surface marked **108b**; and a fifth plastic lens element **110** with negative refractive power having a negative meniscus, with a concave object-side surface marked **110a** and an image-side surface marked **110b**. The optical lens system further comprises an optional glass window **112** disposed between the image-side surface **110b** of fifth lens element **110** and an image plane **114** for image formation of an object. Moreover, an image sensor (not shown) is disposed at image plane **114** for the image formation.

In embodiment **100**, all lens element surfaces are aspheric. Detailed optical data is given in Table 1, and the aspheric surface data is given in Table 2, wherein the units of the radius

TABLE 1

#	Comment	Radius R [mm]	Distances [mm]	Nd/Vd	Diameter [mm]
1	Stop	Infinite	-0.466		2.4
2	L11	1.5800	0.894	1.5345/57.095	2.5
3	L12	-11.2003	0.020		2.4
4	L21	33.8670	0.246	1.63549/23.91	2.2
5	L22	3.2281	0.449		1.9
6	L31	-12.2843	0.290	1.5345/57.095	1.9
7	L32	7.7138	2.020		1.8
8	L41	-2.3755	0.597	1.63549/23.91	3.3
9	L42	-1.8801	0.068		3.6
10	L51	-1.8100	0.293	1.5345/57.095	3.9
11	L52	-5.2768	0.617		4.3
12	Window	Infinite	0.210	1.5168/64.17	3.0
13		Infinite	0.200		3.0

TABLE 2

#	Conic coef- ficient k	α_2	α_3	α_4	α_5	α_6
2	-0.4668	7.9218E-03	2.3146E-02	-3.3436E-02	2.3650E-02	-9.2437E-03
3	-9.8525	2.0102E-02	2.0647E-04	7.4394E-03	-1.7529E-02	4.5206E-03
4	10.7569	-1.9248E-03	8.6003E-02	1.1676E-02	-4.0607E-02	1.3545E-02
5	1.4395	5.1029E-03	2.4578E-01	-1.7734E-01	2.9848E-01	-1.3320E-01
6	0.0000	2.1629E-01	4.0134E-02	1.3615E-02	2.5914E-03	-1.2292E-02
7	-9.8953	2.3297E-01	8.2917E-02	-1.2725E-01	1.5691E-01	-5.9624E-02
8	0.9938	-1.3522E-02	-7.0395E-03	1.4569E-02	-1.5336E-02	4.3707E-03
9	-6.8097	-1.0654E-01	1.2933E-02	2.9548E-04	-1.8317E-03	5.0111E-04
10	-7.3161	-1.8636E-01	8.3105E-02	-1.8632E-02	2.4012E-03	-1.2816E-04
11	0.0000	-1.1927E-01	7.0245E-02	-2.0735E-02	2.6418E-03	-1.1576E-04

of curvature (R), lens element thickness and/or distances between elements along the optical axis and diameter are expressed in mm “Nd” is the refractive index. The equation of the aspheric surface profiles is expressed by:

$$z = \frac{cr^2}{1 + \sqrt{1 - (1+k)c^2r^2}} + \alpha_1 r^2 +$$

$$\alpha_2 r^4 + \alpha_3 r^6 + \alpha_4 r^8 + \alpha_5 r^{10} + \alpha_6 r^{12} + \alpha_7 r^{14}$$

where r is distance from (and perpendicular to) the optical axis, k is the conic coefficient, $c=1/R$ where R is the radius of curvature, and α are coefficients given in Table 2. In the equation above as applied to embodiments of a lens assembly disclosed herein, coefficients α_1 and α_7 are zero. Note that the maximum value of r “max r”=Diameter/2. Also note that Table 1 (and in Tables 3 and 5 below), the distances between various elements (and/or surfaces) are marked “Lmn” (where m refers to the lens element number, n=1 refers to the element thickness and n=2 refers to the air gap to the next element) and are measured on the optical axis z, wherein the stop is at z=0. Each number is measured from the previous surface. Thus, the first distance -0.466 mm is measured from the stop to surface **102a**, the distance L11 from surface **102a** to surface **102b** (i.e. the thickness of first lens element **102**) is 0.894 mm, the gap L12 between surfaces **102b** and **104a** is 0.020 mm, the distance L21 between surfaces **104a** and **104b** (i.e. thickness d2 of second lens element **104**) is 0.246 mm, etc. Also, L21=d₂ and L51=d₅.

Embodiment **100** provides a field of view (FOV) of 44 degrees, with EFL=6.90 mm, F#=2.80 and TTL of 5.904 mm. Thus and advantageously, the ratio TTL/EFL=0.855. Advantageously, the Abbe number of the first, third and fifth lens element is 57.095. Advantageously, the first air gap between lens elements **102** and **104** (the gap between surfaces **102b** and **104a**) has a thickness (0.020 mm) which is less than a tenth of thickness d₂ (0.246 mm). Advantageously, the Abbe number of the second and fourth lens elements is 23.91. Advantageously, the third air gap between lens elements **106** and **108** has a thickness (2.020 mm) greater than TTL/5 (5.904/5 mm). Advantageously, the fourth air gap between lens elements **108** and **110** has a thickness (0.068 mm) which is smaller than 1.5d₅ (0.4395 mm).

The focal length (in mm) of each lens element in embodiment **100** is as follows: f1=2.645, f2=-5.578, f3=-8.784, f4=9.550 and f5=-5.290. The condition $1.2 \times |f3| > |f2| > 1.5 \times f1$ is clearly satisfied, as $1.2 \times 8.787 > 5.578 > 1.5 \times 2.645$. f1 also fulfills the condition $f1 < TTL/2$, as $2.645 < 2.952$.

FIG. 2A shows a second embodiment of an optical lens system disclosed herein and marked **200**. FIG. 2B shows the MTF vs. focus shift of the entire optical lens system for various fields in embodiment **200**. FIG. 2C shows the distortion +Y in percent vs. field. Embodiment **200** comprises in order from an object side to an image side: an optional stop **201**; a first plastic lens element **202** with positive refractive power having a convex object-side surface **202a** and a convex or concave image-side surface **202b**; a second glass lens element **204** with negative refractive power, having a meniscus convex object-side surface **204a**, with an image side surface marked **204b**; a third plastic lens element **206** with negative refractive power having a concave object-side sur-

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face **206a** with an inflection point and a concave image-side surface **206b**; a fourth plastic lens element **208** with positive refractive power having a positive meniscus, with a concave object-side surface marked **208a** and an image-side surface marked **208b**; and a fifth plastic lens element **210** with negative refractive power having a negative meniscus, with a concave object-side surface marked **110a** and an image-side surface marked **210b**. The optical lens system further comprises an optional glass window **212** disposed between the image-side surface **210b** of fifth lens element **210** and an image plane **214** for image formation of an object.

In embodiment **200**, all lens element surfaces are aspheric. Detailed optical data is given in Table 3, and the aspheric surface data is given in Table 4, wherein the markings and units are the same as in, respectively, Tables 1 and 2. The equation of the aspheric surface profiles is the same as for embodiment **100**.

TABLE 3

#	Comment	Radius R [mm]	Distances [mm]	Nd/Vd	Diameter [mm]
1	Stop	Infinite	-0.592		2.5
2	L11	1.5457	0.898	1.53463/56.18	2.6
3	L12	-127.7249	0.129		2.6
4	L21	6.6065	0.251	1.91266/20.65	2.1
5	L22	2.8090	0.443		1.8
6	L31	9.6183	0.293	1.53463/56.18	1.8
7	L32	3.4694	1.766		1.7
8	L41	-2.6432	0.696	1.632445/23.35	3.2
9	L42	-1.8663	0.106		3.6
10	L51	-1.4933	0.330	1.53463/56.18	3.9
11	L52	-4.1588	0.649		4.3
12	Window	Infinite	0.210	1.5168/64.17	5.4
13		Infinite	0.130		5.5

TABLE 4

#	Conic coefficient k	α_2	α_3	α_4	α_5	α_6
2	0.0000	-2.7367E-03	2.8779E-04	-4.3661E-03	3.0069E-03	-1.2282E-03
3	-10.0119	4.0790E-02	-1.8379E-02	2.2562E-02	-1.7706E-02	4.9640E-03
4	10.0220	4.6151E-02	5.8320E-02	-2.0919E-02	-1.2846E-02	8.8283E-03
5	7.2902	3.6028E-02	1.1436E-01	-1.9022E-02	4.7992E-03	-3.4079E-03
6	0.0000	1.6639E-01	5.6754E-02	-1.2238E-02	-1.8648E-02	1.9292E-02
7	8.1261	1.5353E-01	8.1427E-02	-1.5773E-01	1.5303E-01	-4.6064E-02
8	0.0000	-3.2628E-02	1.9535E-02	-1.6716E-02	-2.0132E-03	2.0112E-03
9	0.0000	1.5173E-02	-1.2252E-02	3.3611E-03	-2.5303E-03	8.4038E-04
10	-4.7688	-1.4736E-01	7.6335E-02	-2.5539E-02	5.5897E-03	-5.0290E-04
11	0.00E+00	-8.3741E-02	4.2660E-02	-8.4866E-03	1.2183E-04	7.2785E-05

Embodiment **200** provides a FOV of 43.48 degrees, with EFL=7 mm, F #=2.86 and TTL=5.90 mm. Thus and advantageously, the ratio TTL/EFL=0.843. Advantageously, the Abbe number of the first, third and fifth lens elements is 56.18. The first air gap between lens elements **202** and **204** has a thickness (0.129 mm) which is about half the thickness d_2 (0.251 mm). Advantageously, the Abbe number of the second lens element is 20.65 and of the fourth lens element is 23.35. Advantageously, the third air gap between lens elements **206** and **208** has a thickness (1.766 mm) greater than TTL/5 (5.904/5 mm). Advantageously, the fourth air gap between lens elements **208** and **210** has a thickness (0.106 mm) which is less than $1.5 \times d_5$ (0.495 mm).

The focal length (in mm) of each lens element in embodiment **200** is as follows: $f_1=2.851$, $f_2=-5.468$, $f_3=-10.279$, $f_4=7.368$ and $f_5=-4.536$. $1.2 \times |f_3| > |f_2| > 1.5 \times f_1$ is clearly sat-

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isfied, as $1.2 \times 10.279 > 5.468 > 1.5 \times 2.851$. f_1 also fulfills the condition $f_1 < TTL/2$, as $2.851 < 2.950$.

FIG. **3A** shows a third embodiment of an optical lens system disclosed herein and marked **300**. FIG. **3B** shows the MTF vs. focus shift of the entire optical lens system for various fields in embodiment **300**. FIG. **3C** shows the distortion +Y in percent vs. field. Embodiment **300** comprises in order from an object side to an image side: an optional stop **301**; a first glass lens element **302** with positive refractive power having a convex object-side surface **302a** and a convex or concave image-side surface **302b**; a second plastic lens element **204** with negative refractive power, having a meniscus convex object-side surface **304a**, with an image side surface marked **304b**; a third plastic lens element **306** with negative refractive power having a concave object-side surface **306a** with an inflection point and a concave image-side surface **306b**; a fourth plastic lens element **308** with positive refractive power having a positive meniscus, with a concave object-side surface marked **308a** and an image-side surface marked **308b**; and a fifth plastic lens element **310** with negative refractive power having a negative meniscus, with a concave object-side surface marked **310a** and an image-side surface marked **310b**. The optical lens system further comprises an optional glass window **312** disposed between the image-side surface **310b** of fifth lens element **310** and an image plane **314** for image formation of an object.

In embodiment **300**, all lens element surfaces are aspheric. Detailed optical data is given in Table 5, and the aspheric surface data is given in Table 6, wherein the markings and units are the same as in, respectively, Tables 1 and 2. The equation of the aspheric surface profiles is the same as for embodiments **100** and **200**.

TABLE 5

#	Comment	Radius R [mm]	Distances [mm]	Nd/Vd	Diameter [mm]
1	Stop	Infinite	-0.38		2.4
2	L11	1.5127	0.919	1.5148/63.1	2.5
3	L12	-13.3831	0.029		2.3
4	L21	8.4411	0.254	1.63549/23.91	2.1
5	L22	2.6181	0.426		1.8
6	L31	-17.9618	0.265	1.5345/57.09	1.8
7	L32	4.5841	1.998		1.7
8	L41	-2.8827	0.514	1.63549/23.91	3.4
9	L42	-1.9771	0.121		3.7
10	L51	-1.8665	0.431	1.5345/57.09	4.0
11	L52	-6.3670	0.538		4.4
12	Window	Infinite	0.210	1.5168/64.17	3.0
13		Infinite	0.200		3.0

TABLE 6

#	Conic coef- ficient k	α_2	α_3	α_4	α_5	α_6
2	-0.534	1.3253E-02	2.3699E-02	-2.8501E-02	1.7853E-02	-4.0314E-03
3	-13.473	3.0077E-02	4.7972E-03	1.4475E-02	-1.8490E-02	4.3565E-03
4	-10.132	7.0372E-04	1.1328E-01	1.2346E-03	-4.2655E-02	8.8625E-03
5	5.180	-1.9210E-03	2.3799E-01	-8.8055E-02	2.1447E-01	-1.2702E-01
6	0.000	2.6780E-01	1.8129E-02	-1.7323E-02	3.7372E-02	-2.1356E-02
7	10.037	2.7660E-01	-1.0291E-02	-6.0955E-02	7.5235E-02	-1.6521E-02
8	1.703	2.6462E-02	-1.2633E-02	-4.7724E-04	-3.2762E-03	1.6551E-03
9	-1.456	5.7704E-03	-1.8826E-02	5.1593E-03	-2.9999E-03	8.0685E-04
10	-6.511	-2.1699E-01	1.3692E-01	-4.2629E-02	6.8371E-03	-4.1415E-04
11	0.000	-1.5120E-01	8.6614E-02	-2.3324E-02	2.7361E-03	-1.1236E-04

Embodiment **300** provides a FOV of 44 degrees, EFL=6.84 mm, F #=-2.80 and TTL=5.904 mm. Thus and advantageously, the ratio TTL/EFL=0.863. Advantageously, the Abbe number of the first lens element is 63.1, and of the third and fifth lens elements is 57.09. The first air gap between lens elements **302** and **304** has a thickness (0.029 mm) which is about $\frac{1}{10}^{th}$ the thickness d_2 (0.254 mm). Advantageously, the Abbe number of the second and fourth lens elements is 23.91. Advantageously, the third air gap between lens elements **306** and **308** has a thickness (1.998 mm) greater than TTL/5 (5.904/5 mm). Advantageously, the fourth air gap between lens elements **208** and **210** has a thickness (0.121 mm) which is less than $1.5d_s$ (0.6465 mm).

The focal length (in mm) of each lens element in embodiment **300** is as follows: $f_1=2.687$, $f_2=-6.016$, $f_3=-6.777$, $f_4=8.026$ and $f_5=-5.090$. $1.2 \times |f_3| > |f_2| > 1.5 \times f_1$ is clearly satisfied, as $1.2 \times 6.777 > 6.016 > 1.5 \times 2.687$. f_1 also fulfills the condition $f_1 < TTL/2$, as $2.687 < 2.952$.

While this disclosure has been described in terms of certain embodiments and generally associated methods, alterations and permutations of the embodiments and methods will be apparent to those skilled in the art. The disclosure is to be understood as not limited by the specific embodiments described herein, but only by the scope of the appended claims.

The invention claimed is:

1. A lens assembly, comprising: a plurality of refractive lens elements arranged along an optical axis, wherein at least one surface of at least one of the plurality of lens elements is aspheric, wherein the lens assembly has an effective focal length (EFL), and wherein the lens assembly has a total track length (TTL) of 6.5 millimeters or less and a ratio TTL/EFL of less than 1.0, wherein the plurality of lens elements comprises, in order from an object side to an image side, a first lens element with positive refractive power and a second lens element with negative refractive power, wherein a focal length f_1 of the first lens element is smaller than TTL/2.

2. The lens assembly of claim 1, wherein the plurality of lens elements further comprises, in order from an object side to an image side, a third lens element with negative refractive power, and a fourth element, wherein the third and fourth lens elements are separated by an air gap which is greater than TTL/5.

3. The lens assembly of claim 2, wherein the plurality of lens elements further comprises a fifth lens element, wherein one of the fourth and the fifth lens elements has a positive refractive power and the other of the fourth and fifth lens elements has a negative refractive power.

4. The lens assembly of claim 3, wherein the fourth lens element and the fifth lens element are separated by a second air gap which is smaller than TTL/20.

5. The lens assembly of claim 4, wherein a focal length f_1 of the first lens element is smaller than TTL/2.

6. The lens assembly of claim 4, wherein a lens assembly F # is smaller than 2.9.

7. The lens assembly of claim 6, wherein the first lens element has an Abbe number greater than 50 and the second lens element has an Abbe number smaller than 30.

8. The lens assembly of claim 7, wherein one of the fourth and fifth lens elements that has a positive refractive power is characterized by an Abbe number smaller than 30 and wherein the other of the fourth and fifth lens elements that has a negative refractive power is characterized by an Abbe number greater than 50, thereby adding compensation for chromatic aberrations and assisting in bringing all fields focal points to an image plane.

9. The lens assembly of claim 8, wherein the third, fourth and fifth lens element are made of plastic.

10. The lens assembly of claim 8, wherein all the lens elements are made of plastic.

11. The lens assembly of claim 8, wherein the first lens element has a convex object-side surface and a convex or concave image-side surface and wherein the second lens element is a meniscus lens having a convex object-side surface.

12. The lens assembly of claim 11, wherein the focal length f_1 , a focal length f_2 of the second lens element and a focal length f_3 of the third lens element fulfill the condition $1.2 \times |f_3| > |f_2| > 1.5 \times f_1$.

13. The lens assembly of claim 1, wherein the first lens element has an Abbe number greater than 50 and the second lens element has an Abbe number smaller than 30.

14. The lens assembly of claim 13, wherein the first lens element has a convex object-side surface and a convex or concave image-side surface and wherein the second lens element is a meniscus lens having a convex object-side surface.

15. The lens assembly of claim 14, wherein a lens assembly F # is smaller than 2.9.

16. The lens assembly of claim 15, wherein the plurality of lens elements further comprises a third lens element with negative refractive power, a fourth lens element and a fifth lens element, wherein one of the fourth and fifth lens elements has a positive refractive power and the other of the fourth and the fifth lens elements has a negative refractive power.

17. The lens assembly of claim 16, wherein the third, fourth and fifth lens element are made of plastic, and wherein the fourth and fifth lens elements are separated by a second air gap which is smaller than TTL/20.

18. The lens assembly of claim 16, wherein one of the fourth and fifth lens elements that has a positive refractive power is characterized by an Abbe number smaller than 30 and wherein the other lens element of the fourth and fifth lens elements that has a negative refractive power is characterized by an Abbe number greater than 50, thereby adding compen-

sation for chromatic aberrations and assisting in bringing all fields focal points to an image plane.

19. The lens assembly of claim **18**, wherein the focal length f_1 , a focal length f_2 of the second lens element and a focal length f_3 of the third lens element fulfill the condition $1.2 \times |f_3| > |f_2| > 1.5 \times f_1$.

20. A lens assembly having a total track lens (TTL) smaller than an effective focal length (EFL) thereof and comprising: a plurality of lens elements made of at least two different polymer materials having different Abbe numbers and including, in order from an object plane to an image plane along an optical axis of the lens assembly, a first lens element having positive optical power and a pair of second and third lenses having each a negative optical power, the combination of the first, second and third lens elements providing the lens assembly with a ratio $TTL/EFL < 1$, wherein the second and third lens elements are each made of a different one of the at least two polymer materials having a different Abbe number to reduce chromatic aberrations of the lens assembly, the plurality of lens elements further including a combination of fourth and fifth lens elements configured to assist in bringing all fields focal points to the image plane, wherein the third and fourth lens elements are separated by an air gap which is greater than $TTL/5$, and wherein the fourth and fifth lens elements are each made of a different one of the at least two polymer materials having a different Abbe number to further reduce chromatic aberrations of the lens assembly.

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